

THz generation and transport

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Overview

- Motivation
- Design goals
- Simulation tools
 - POP ZEMAX
 - Mathematica code (B. Schmidt, DESY)
- THz beam extraction
- Optical design
- Simulation of the THz radiation transfer line
- Summary and outlook

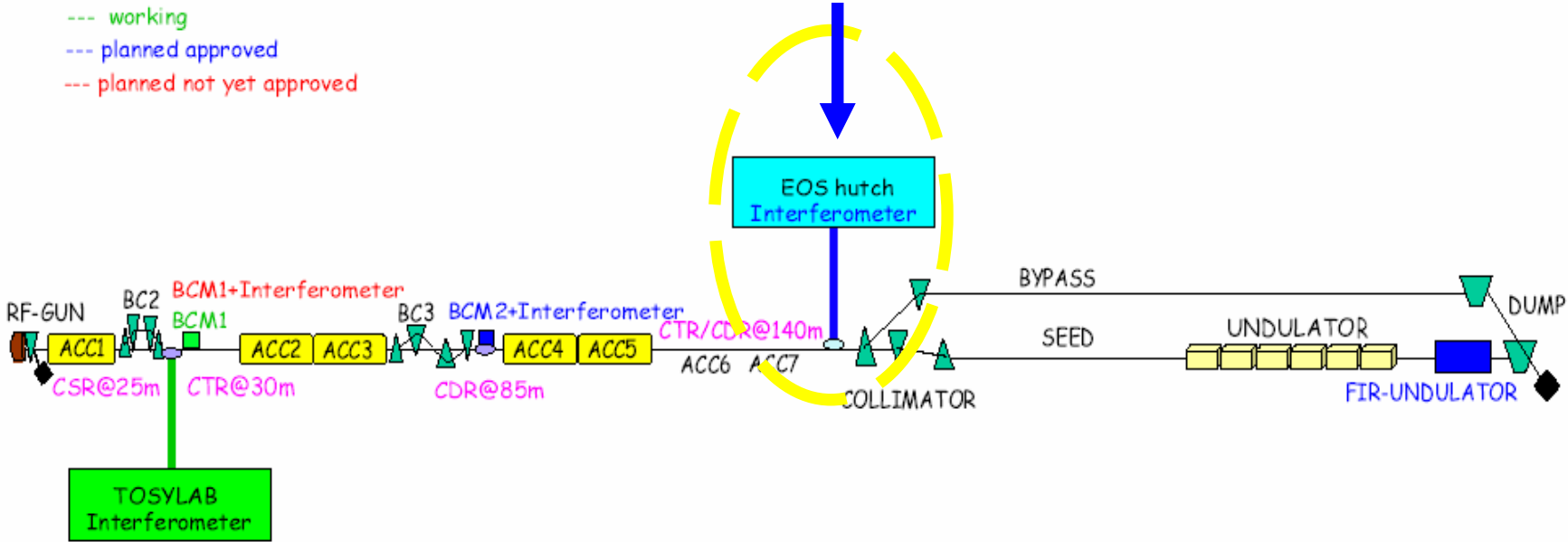
Motivation

Bunch length measurements with interferometer

CTR=Coherent Transition Radiation
 CDR=Coherent Diffraction Radiation
 CSR=Coherent Synchrotron Radiation

--- working
 --- planned approved
 --- planned not yet approved

CDR/CTR
 140 m, $\gamma = 1000$, $E_{el} = 500$ MeV



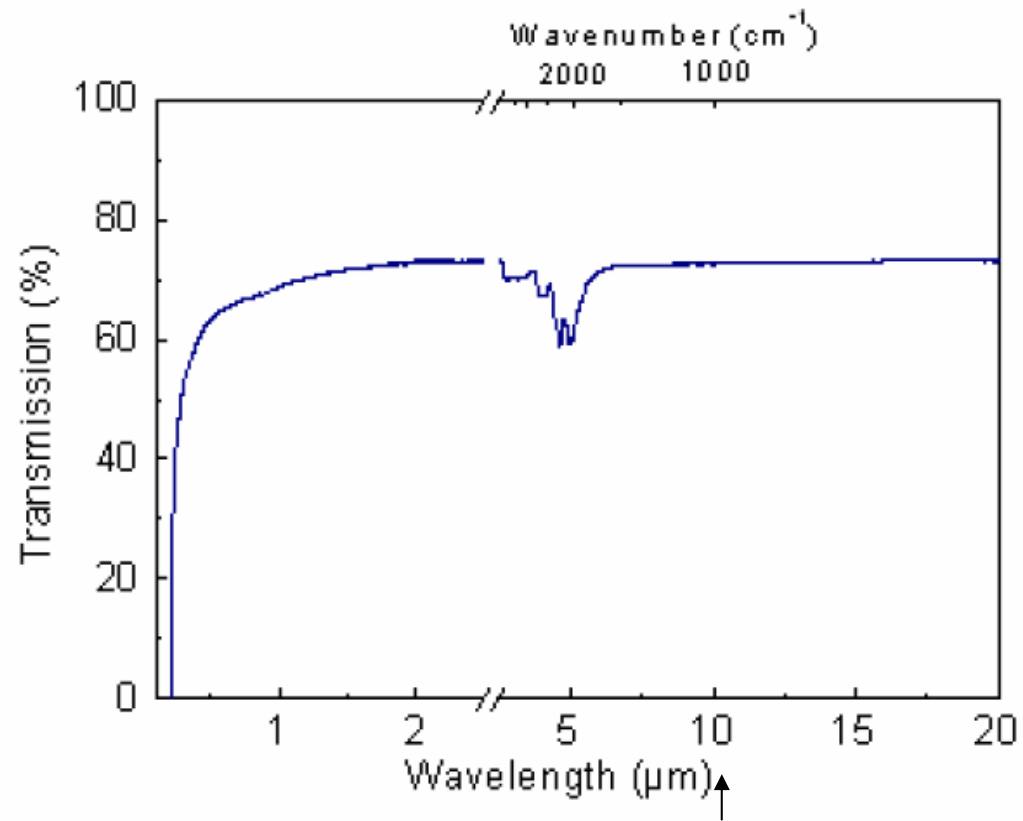
○ z-cut quartz window
 ○ diamond window (planned)
 BCM=Bunch Compressor Monitor

~5m

Design goals

- Flat frequency response
- Low frequency response limit as low as possible BUT
 - Finite dimensions of transfer line tube and mirrors ($\phi \approx 200\text{mm}$)
 - Long transfer line $\sim 20\text{m}$
- High frequency structures expected from μ bunching up to $30\text{THz}(10\mu\text{m})$

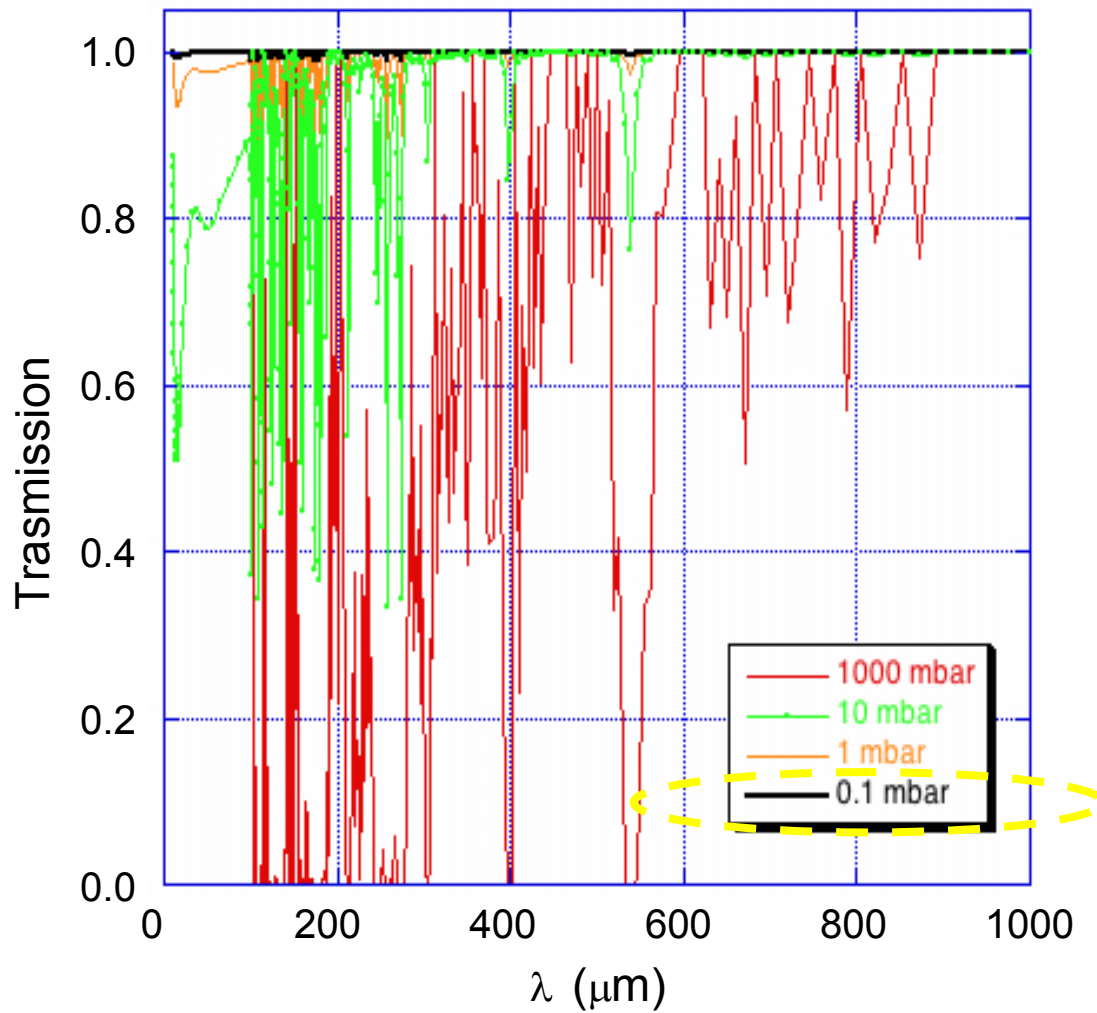
Diamond window



Optical transmission spectrum of CVD diamond
30THz

Vacuum needed

Transmission through 20m of Humid Air (50% RH)



from B. Schmidt

S. Casalbuoni, DESY

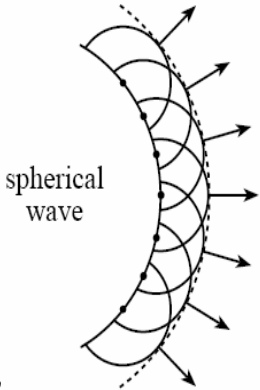
Simulation Tools

2 CODES

ZEMAX
 Commercially available
 POP (Physical Optic Propagation)

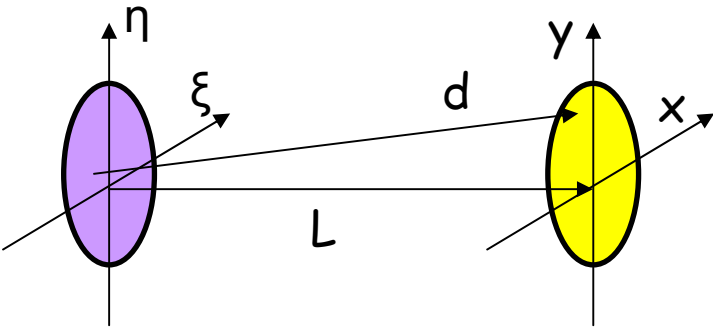
B. Schmidt (DESY)
 Mathematica

Huygens-Fresnel principle:
 Every point of a wave front may be considered as a centre of a secondary disturbance which gives rise to spherical wavelets, and the wave-front at any later instant may be regarded as the envelope of these wavelets. The secondary wavelets mutually interfere.



Kirchhoff integral

$$\tilde{E}(x, y, L, \omega) = \iint_{\text{Surf}(\xi, \eta)} \tilde{E}(\xi, \eta, 0, \omega) \frac{e^{ikd}}{i\lambda d} d\xi d\eta$$



finite size
screen

$$d^2 = L^2 + (x - \xi)^2 + (y - \eta)^2; d = L \sqrt{1 + \left(\frac{x - \xi}{L}\right)^2 + \left(\frac{y - \eta}{L}\right)^2}$$

$$|x - \xi|, |y - \eta| \ll L$$

$$d \cong L + \frac{x^2 + y^2}{2L} - \frac{x\xi + y\eta}{L} + \frac{\xi^2 + \eta^2}{2L}$$

first order
Fraunhofer

second order
near field, Fresnel

Input for CTR

Fourier Transform with respect to the longitudinal coordinate $\zeta=z-vt$ of the radial electric field \tilde{E}_r of a uniform bunch charge distribution of radius ρ moving with velocity v in straight line uniform motion (M. Geitz, PhD Thesis).

r = radial coordinate ρ = beam radius b = pipe radius $k = 2\pi / \lambda = \omega / c$

$$\tilde{E}_r(k, r) = r \cdot I_1(kr/\gamma) \cdot K_1(k\rho/\gamma) + \rho \cdot I_1(kr/\gamma) \cdot I_1(k\rho/\gamma) \frac{K_0(kb/\gamma)}{I_0(kb/\gamma)}; \quad r < \rho$$

$$\tilde{E}_r(k, r) = \rho \cdot I_1(k\rho/\gamma) \cdot K_1(kr/\gamma) + \rho \cdot I_1(kr/\gamma) \cdot I_1(k\rho/\gamma) \frac{K_0(kb/\gamma)}{I_0(kb/\gamma)}; \quad r > \rho$$

$$\varphi = \text{atan}(y/x)$$

$$\tilde{E}_x = \tilde{E}_r \cdot \cos \varphi \quad \tilde{E}_y = \tilde{E}_r \cdot \sin \varphi$$

Ginzburg-Frank

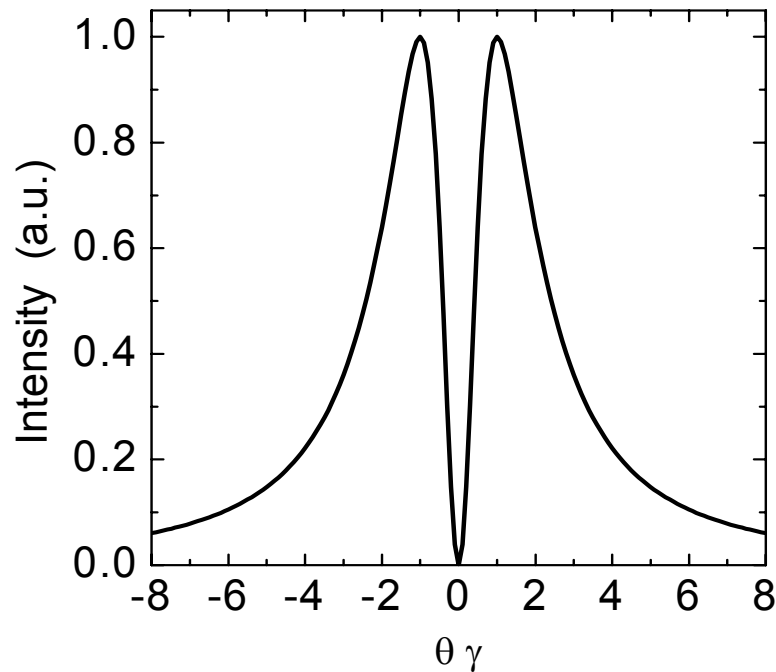
Valid: - if CTR screen radius \geq effective CTR radius

$$a \geq \lambda \gamma$$

-if $L \gg \lambda \gamma^2 \Rightarrow$ far field

(Castellano & Verzilov, Phy.Rev.ST-Accel. Beams ,1998)

$$I(x/L) \propto \frac{\beta^2 \sin^2(x/L)}{(1 - \beta^2 \sin^2(x/L))} \quad \frac{x}{L} = \theta \Rightarrow \text{frequency independent}$$



$\gamma \approx 100$ radius CTR screen [m]: $a = 30\text{mm}$

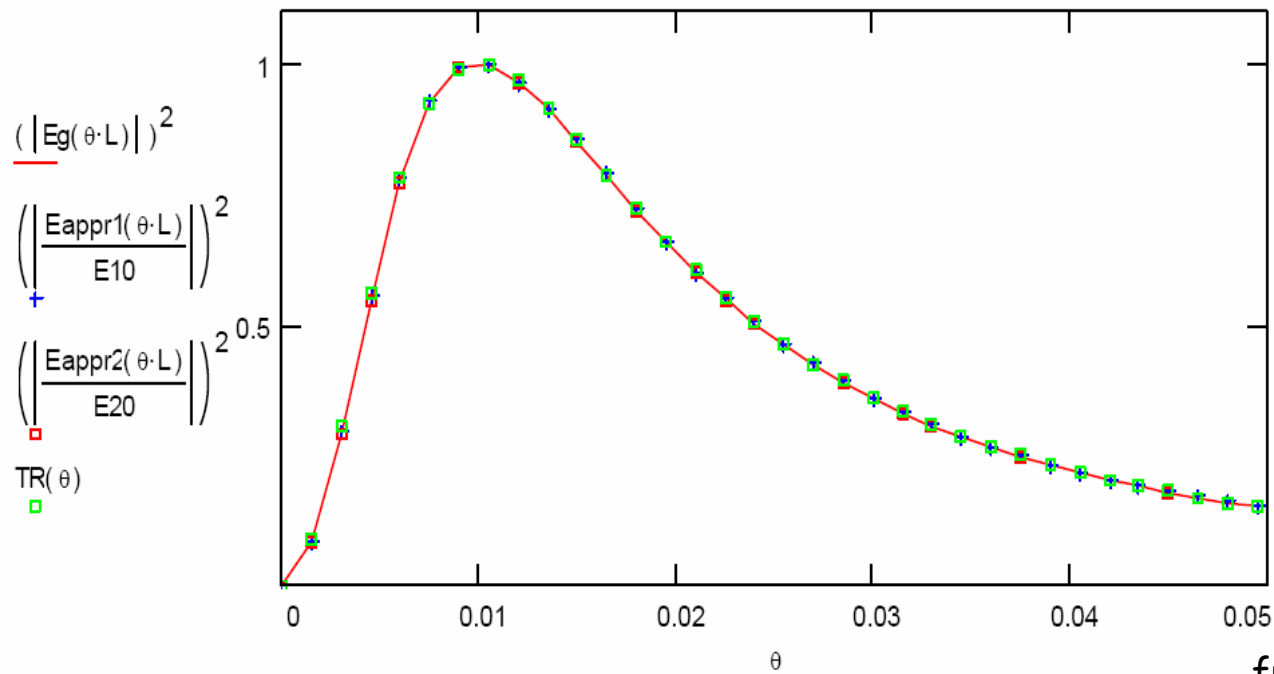
distance to observation screen [m]: $L = 10\text{m}$

wavelength $\lambda = 300\mu\text{m}$

$$\gamma \frac{\lambda}{a} = 1 \qquad \frac{L}{\gamma^2 \cdot \lambda} = 3.333$$

Both conditions satisfied

green: Ginzburg-Frank blue: first order, red: exact SQRT resp. second order



from P. Schmüser

S. Casalbuoni, DESY

$\gamma \approx 100$

radius CTR screen [m]: $a = 30\text{mm}$

distance to observation screen [m]: $L = 20\text{m}$

wavelength

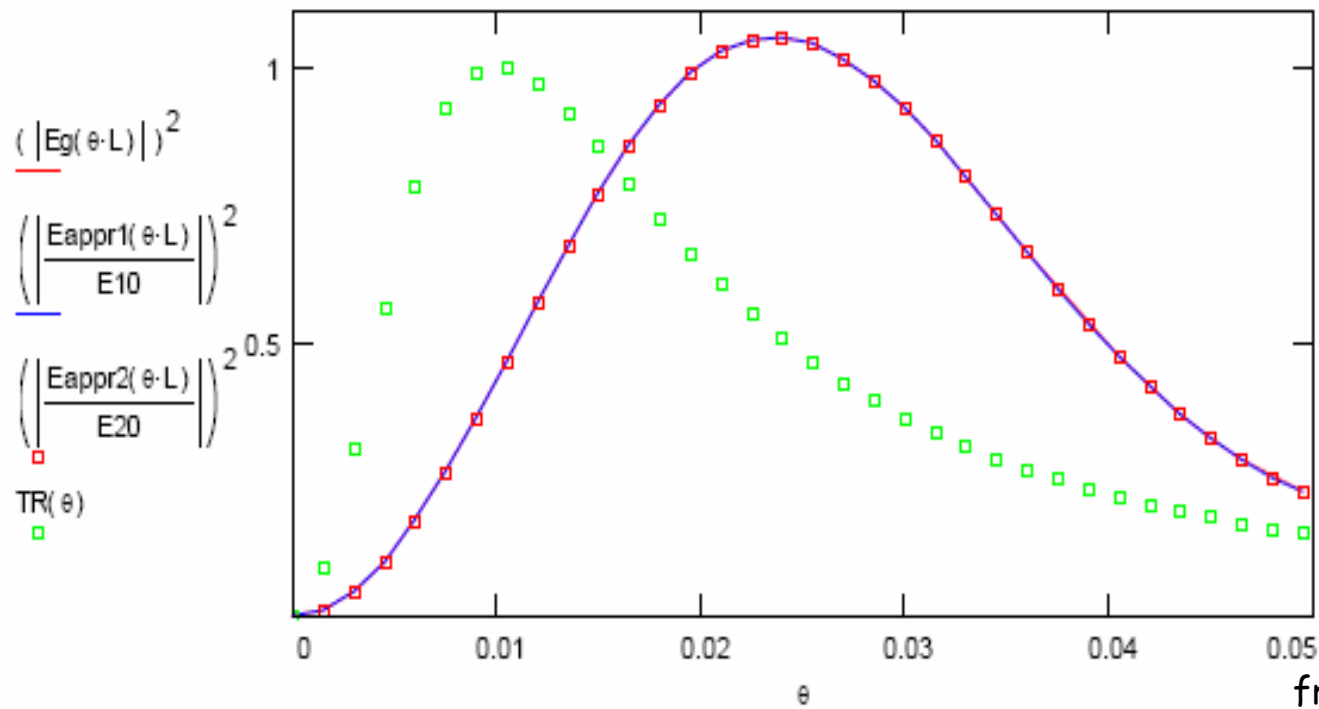
$\lambda = 1.5\text{mm}$

Finite size
CTR screen

$$\gamma \frac{\lambda}{a} = 5$$

$$\frac{L}{\gamma \cdot \lambda} = 1.333$$

green: Ginzburg-Frank, blue: first order, red: exact SQRT resp. second order



from P. Schmüser

S. Casalbuoni, DESY

$\gamma \approx 100$

radius CTR screen [m]: $a = 30\text{mm}$

distance to observation screen [m]: $L = 0.5\text{m}$

wavelength

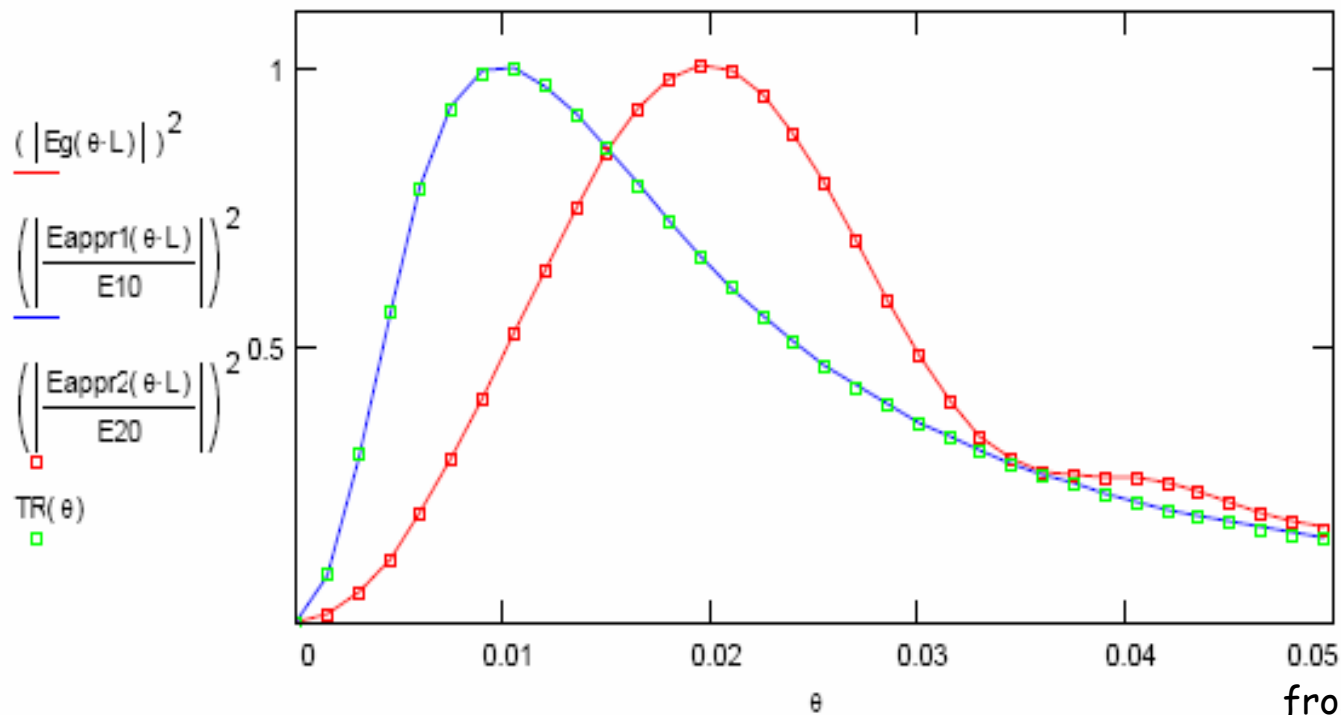
$\lambda = 300\mu\text{m}$

$$\gamma \frac{\lambda}{a} = 1$$

$$\frac{L}{\gamma \cdot \lambda} = 0.167$$

Near field

green: Ginzburg-Frank, blue: first order, red: exact SQRT resp. second order



from P. Schmüser

S. Casalbuoni, DESY

$$\gamma = 100$$

$$L = 0.5\text{m}$$

$$a = 30\text{mm}$$

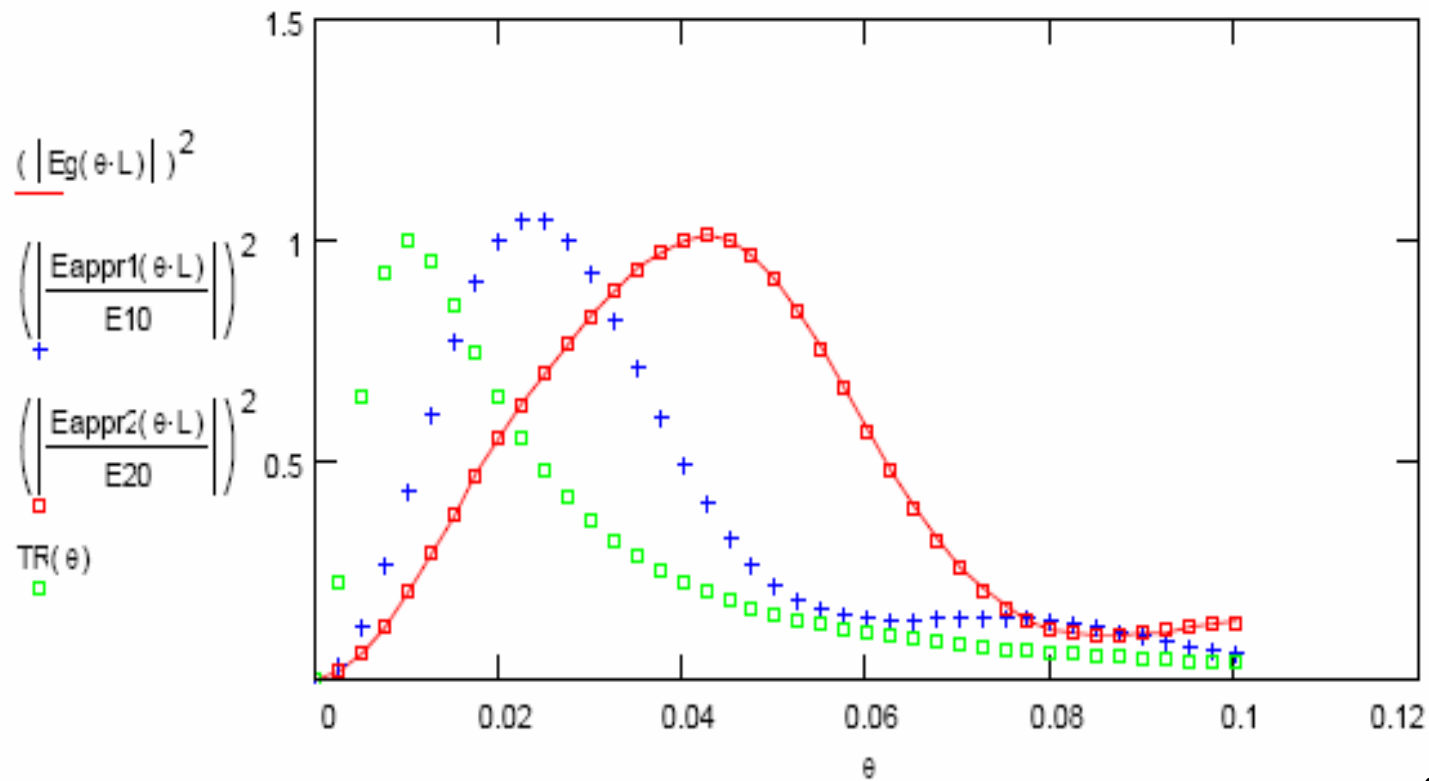
$$\lambda = 1.5\text{mm}$$

$$\frac{\lambda \cdot \gamma}{a} = 5$$

$$\frac{L}{\lambda \cdot \gamma^2} = 0.033$$

Both conditions
violated

green: Ginzburg-Frank, blue first order, red: second order and exact SQRT



from P. Schmüser
S. Casalbuoni, DESY

Simulation Tools

2 CODES

ZEMAX

Commercially available

POP (Physical Optic Propagation)

B. Schmidt (DESY)

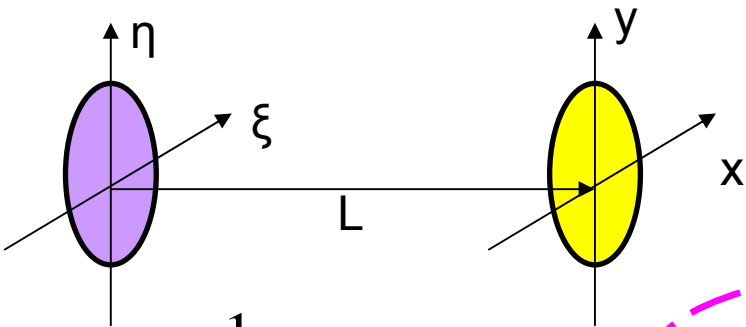
Mathematica

Both make use of scalar Fresnel diffraction theory

Valid if objects and apertures $\gg \lambda$ $|x-\xi|, |y-\eta| \ll L$

$$\tilde{E}(x, y, L, \omega) = \frac{1}{i\lambda d} \iint_{\text{Surf}(\xi, \eta)} \tilde{E}(\xi, \eta, 0, \omega) e^{ikd} d\xi d\eta$$

Fourier transform of



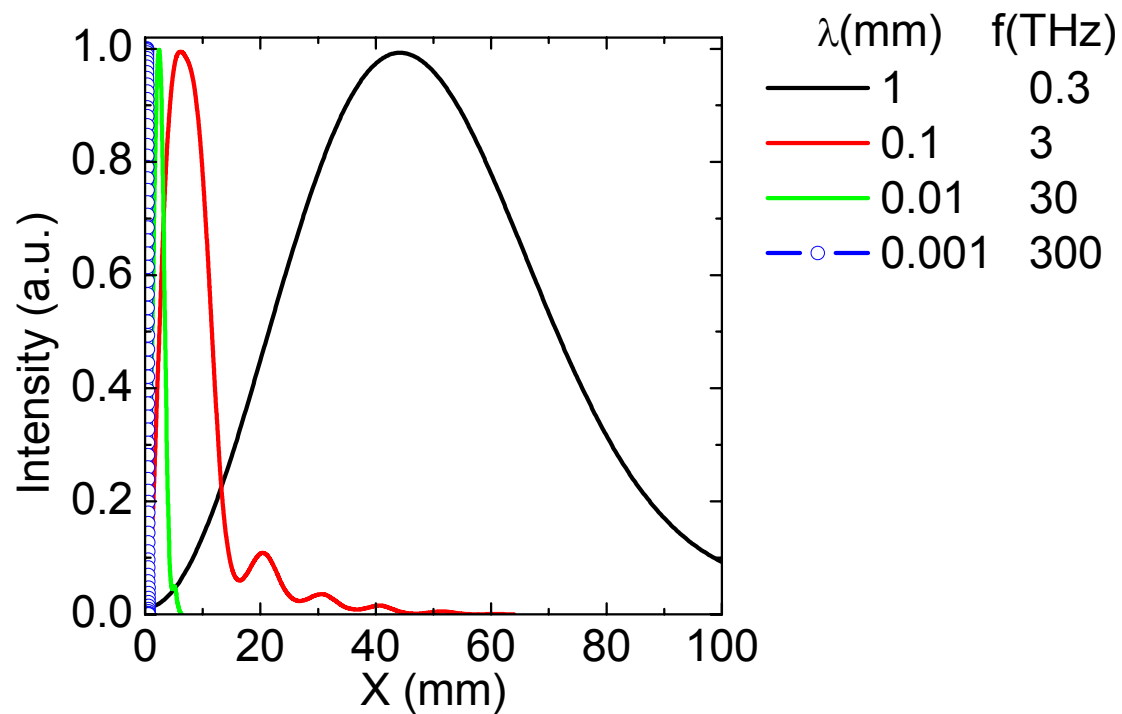
$$\tilde{E}(x, y, L, \omega) = \frac{1}{i\lambda L} e^{ik(x^2+y^2)/2L} \iint_{\text{Surf}(\xi, \eta)} \tilde{E}(\xi, \eta, 0, \omega) e^{ik(\xi^2+\eta^2)/2L} e^{ik(x\xi+y\eta)/2L} d\xi d\eta$$

$$k = \frac{2\pi}{\lambda}; \quad \lambda = \frac{2\pi c}{\omega}$$

Free propagation

if $a \lesssim \gamma\lambda$ and/or $L \lesssim \lambda \gamma^2 \Rightarrow I(x, L, \omega)$ frequency dependent

$L=1$ m; $a=10$ mm; $\gamma=1000$



Dimensions of the CTR screen

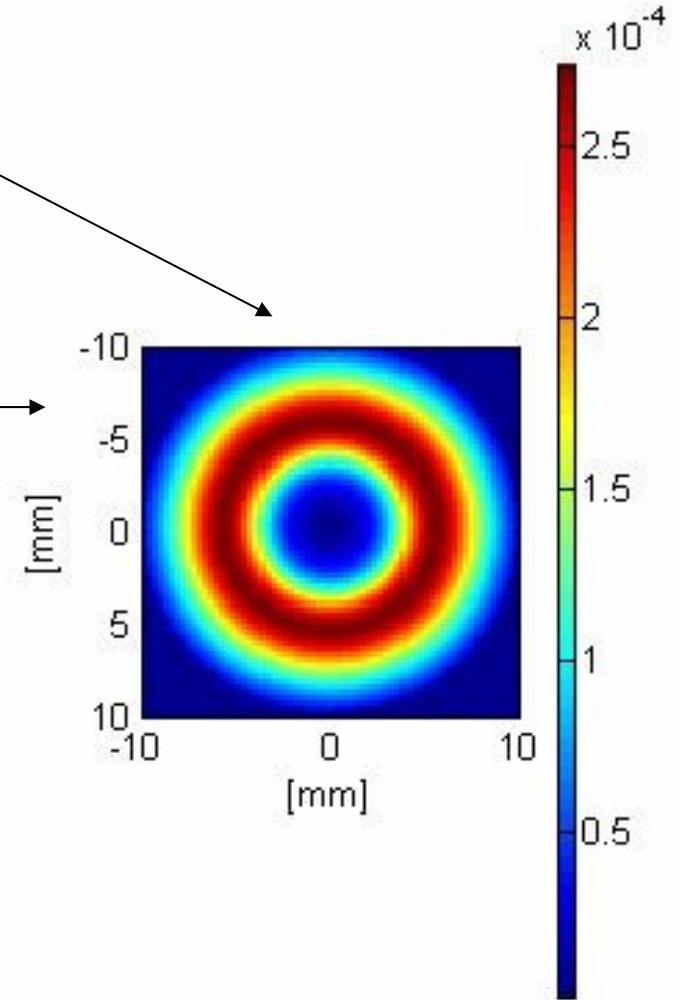
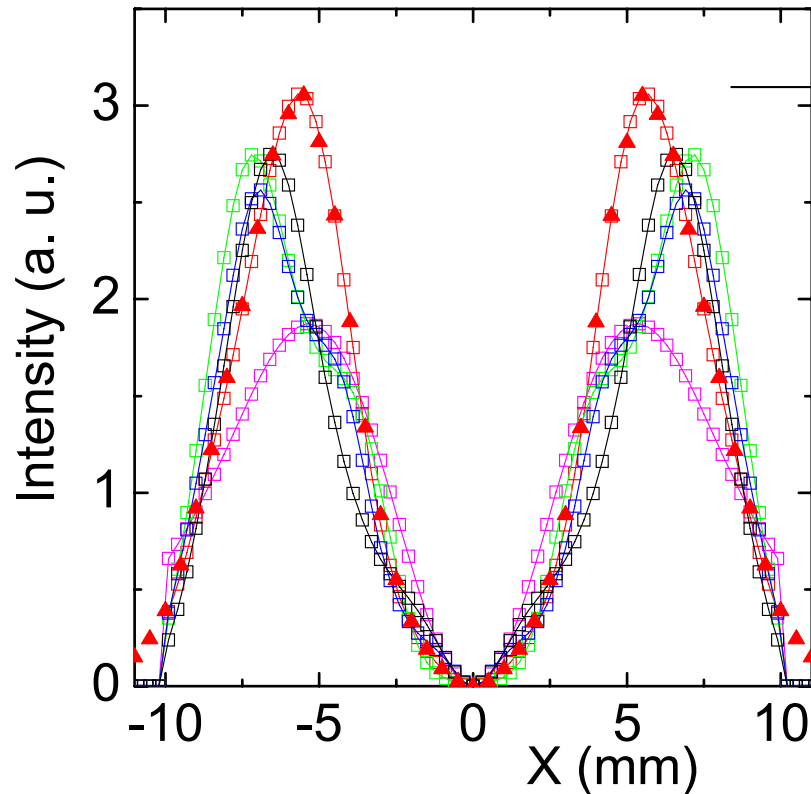
window $\phi=20\text{mm}$
 $L=40\text{mm}; \gamma=1000$
 $\lambda=1.5\text{mm} \Rightarrow f=200\text{GHz}$

screen intensity @window/@screen

ϕ (mm)

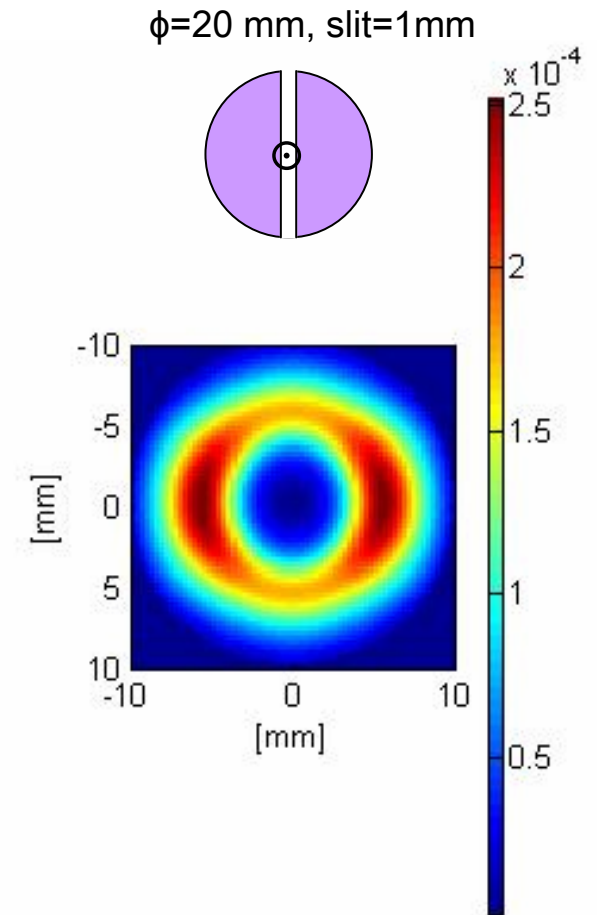
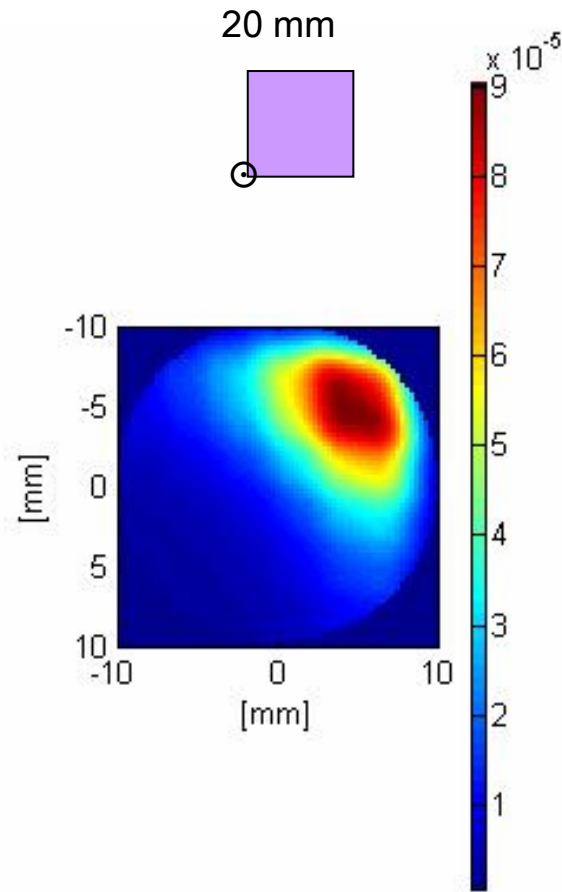
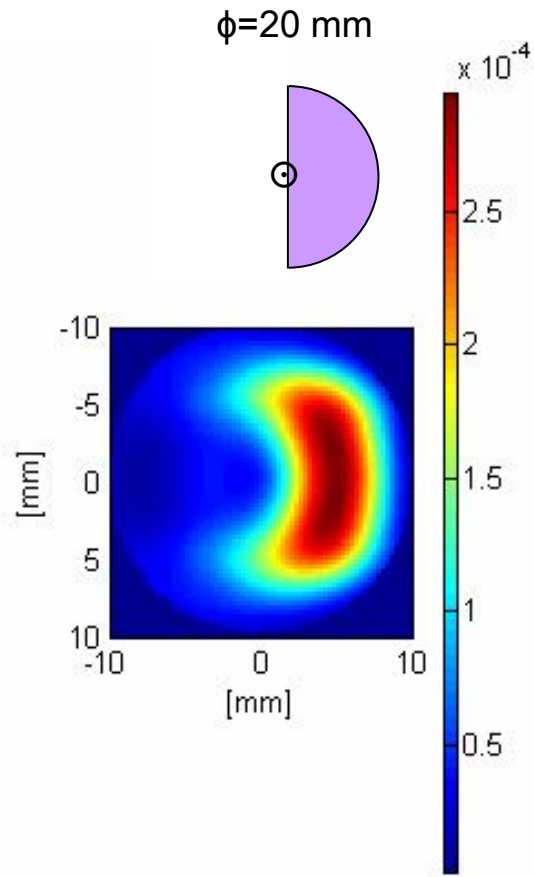
10	0.74
20	0.84
25	0.83
30	0.79
40	0.70

—□— ZEMAX
▲ Mathematica



window $\phi=20\text{mm}$
 $L=40\text{mm}$; $\gamma=1000$
 $\lambda=1.5\text{mm} \Rightarrow f=200\text{GHz}$

CDR screen

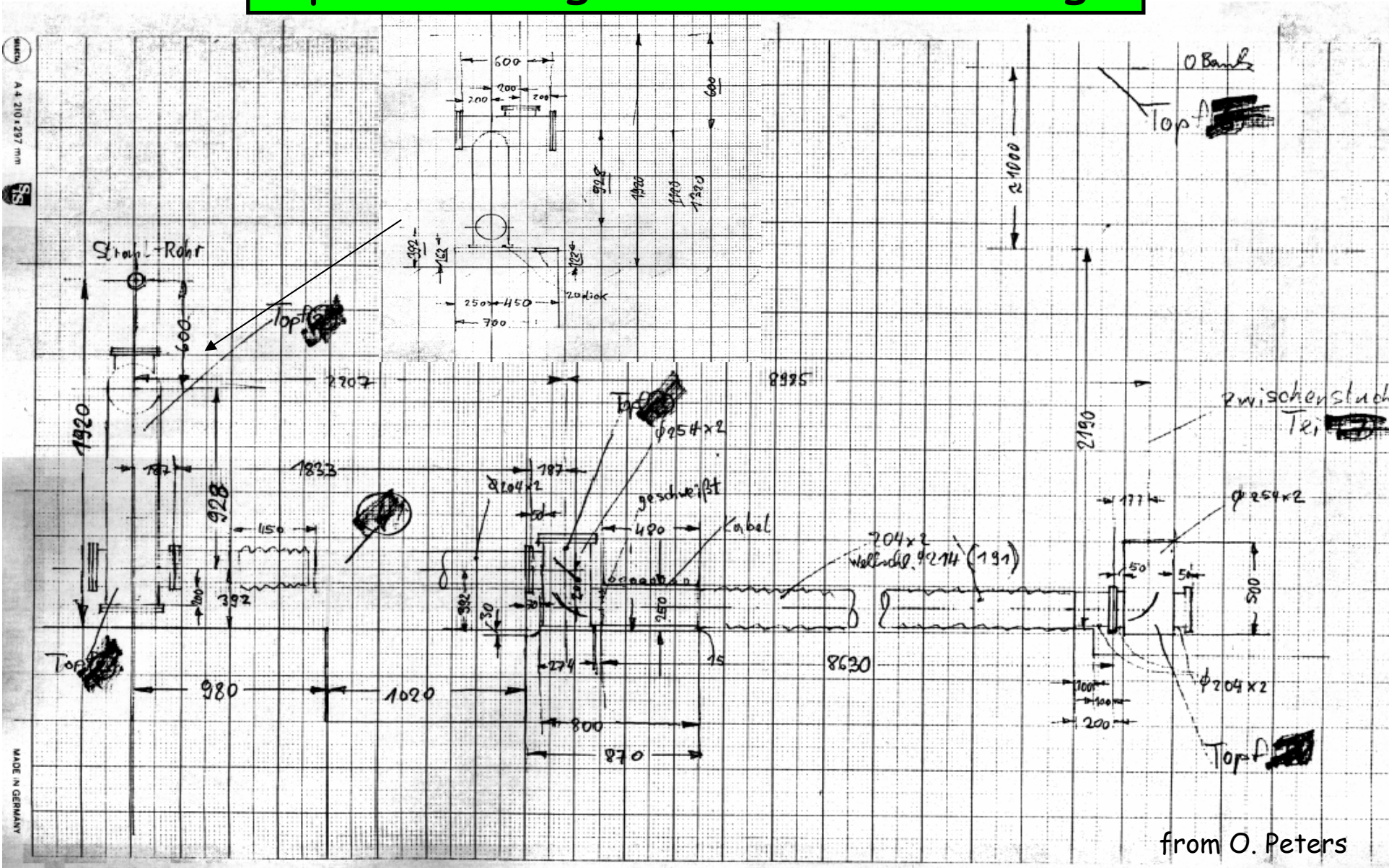


intensity
@window/@screen
0.75

0.55

0.78

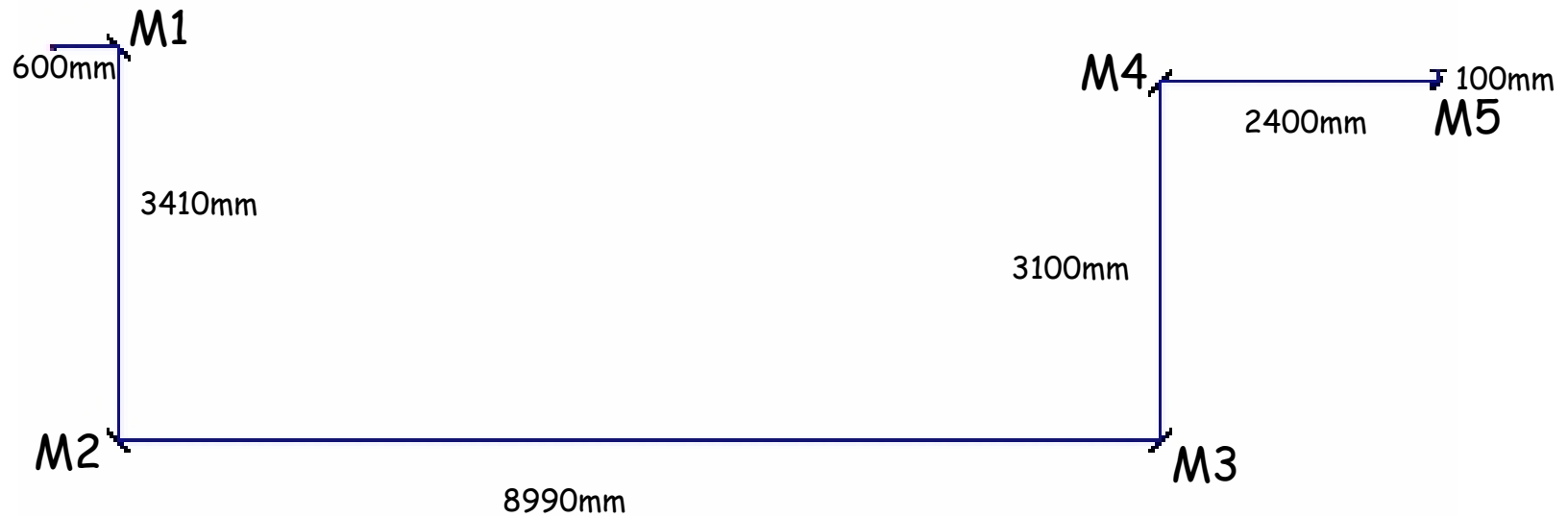
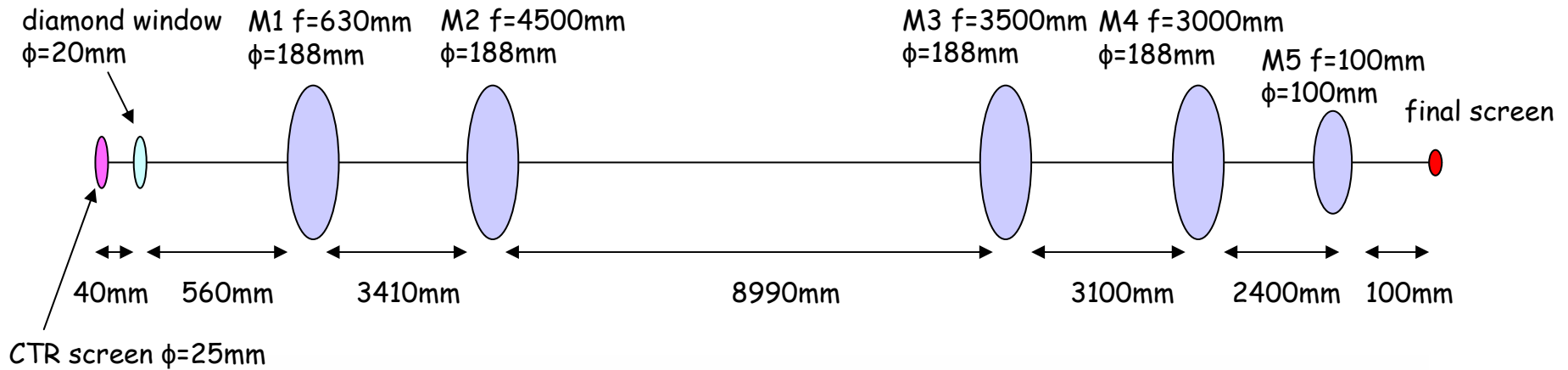
Optical design: technical drawing



from O. Peters

S. Casalbuoni, DESY

Optical design



Simulation of the THz radiation transfer line with ideal thin lenses

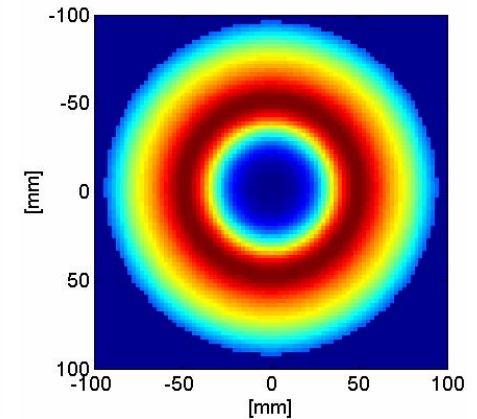
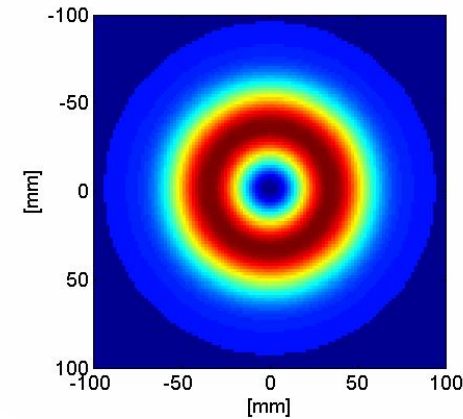
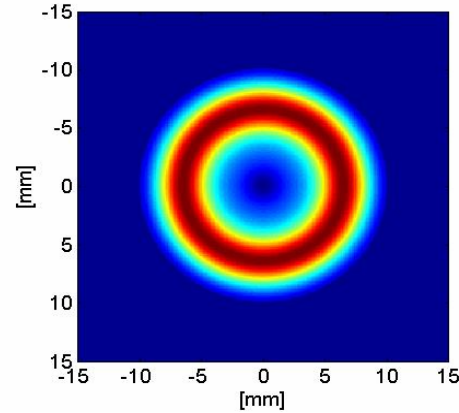
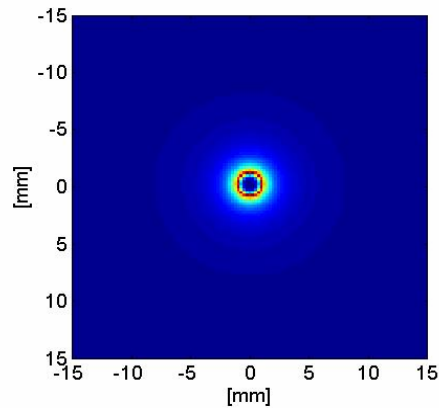
$\lambda=1.5\text{mm} \Rightarrow f=200\text{GHz}; \gamma=1000$

CTR screen $\phi=25\text{mm}$

Diamond window $\phi=20\text{mm}$

M1

M2

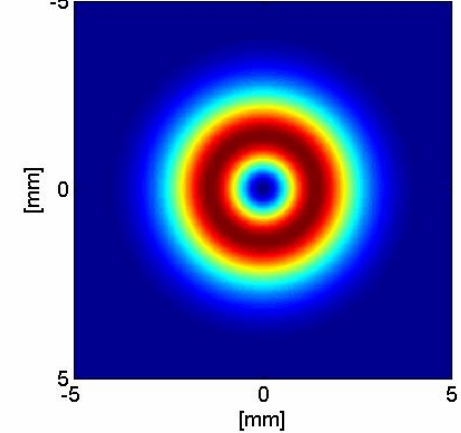
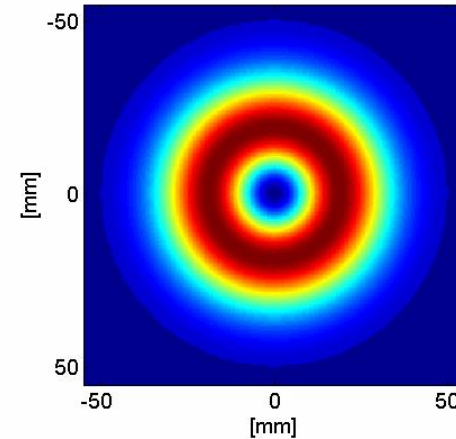
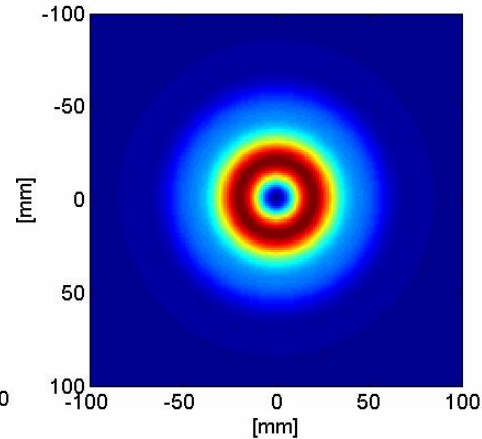
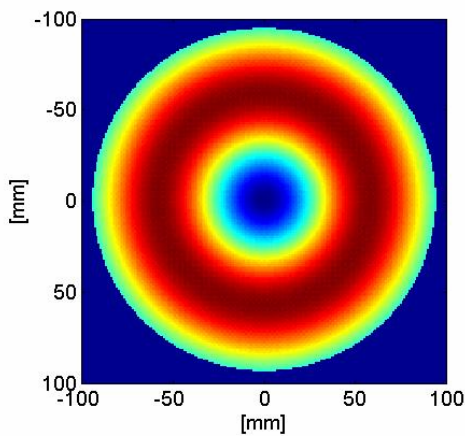


M3

M4

M5

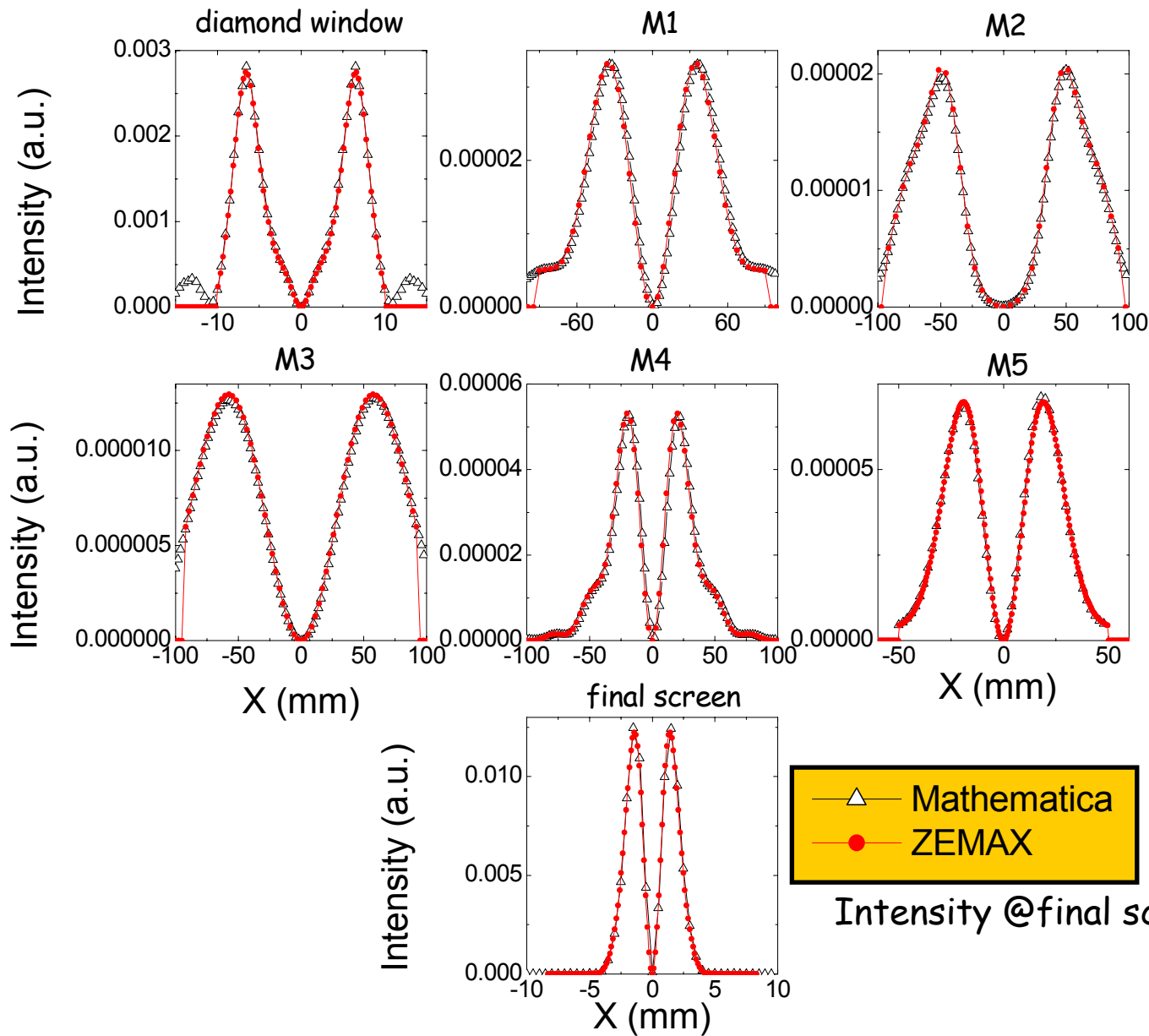
final screen $\phi=8\text{mm}$



Intensity @final screen/@window=0.49

S. Casalbuoni, DESY

Simulation of the THz radiation transfer line with ideal thin lenses

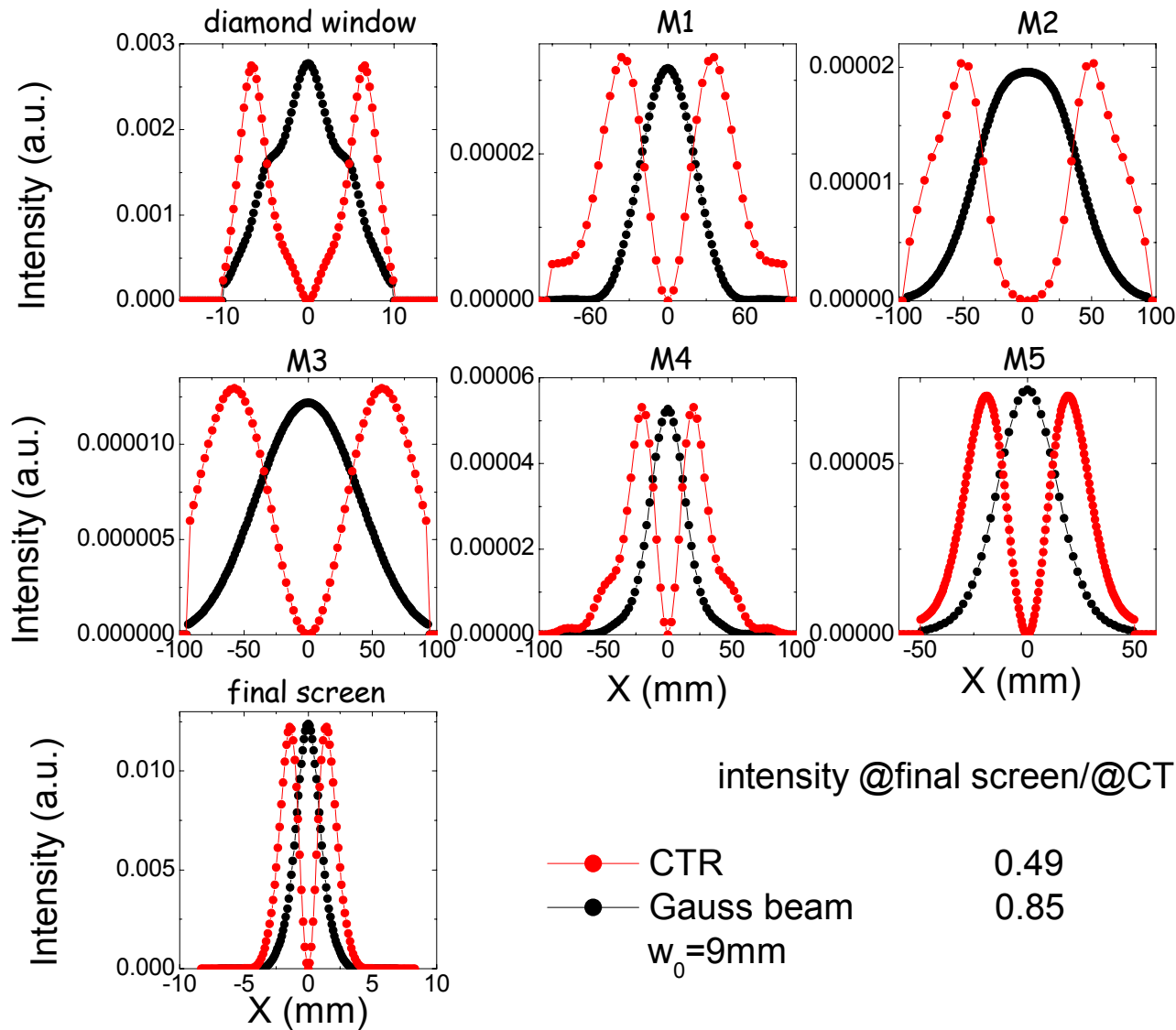


$\lambda = 1.5\text{mm} \Rightarrow f = 200\text{GHz}$
 $\gamma = 1000$
 $\text{CTR}_{\text{screen}} \phi = 25\text{mm}$
 $\text{Diamond window } \phi = 20\text{mm}$

—△— Mathematica
 —●— ZEMAX

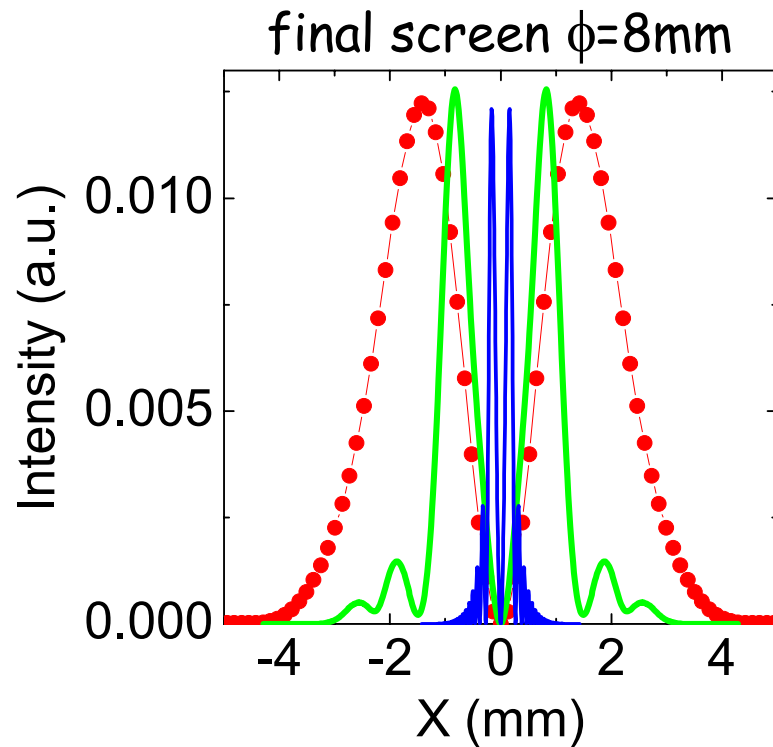
Intensity @final screen/@window=0.49

Good also for a Gaussian beam



$\lambda = 1.5\text{mm} \Rightarrow f = 200\text{GHz}$
 $\gamma = 1000$
 $\text{CTR}_{\text{screen}} \phi = 25\text{mm}$
 Diamond window $\phi = 20\text{mm}$

Simulation of the THz radiation transfer line at different frequencies



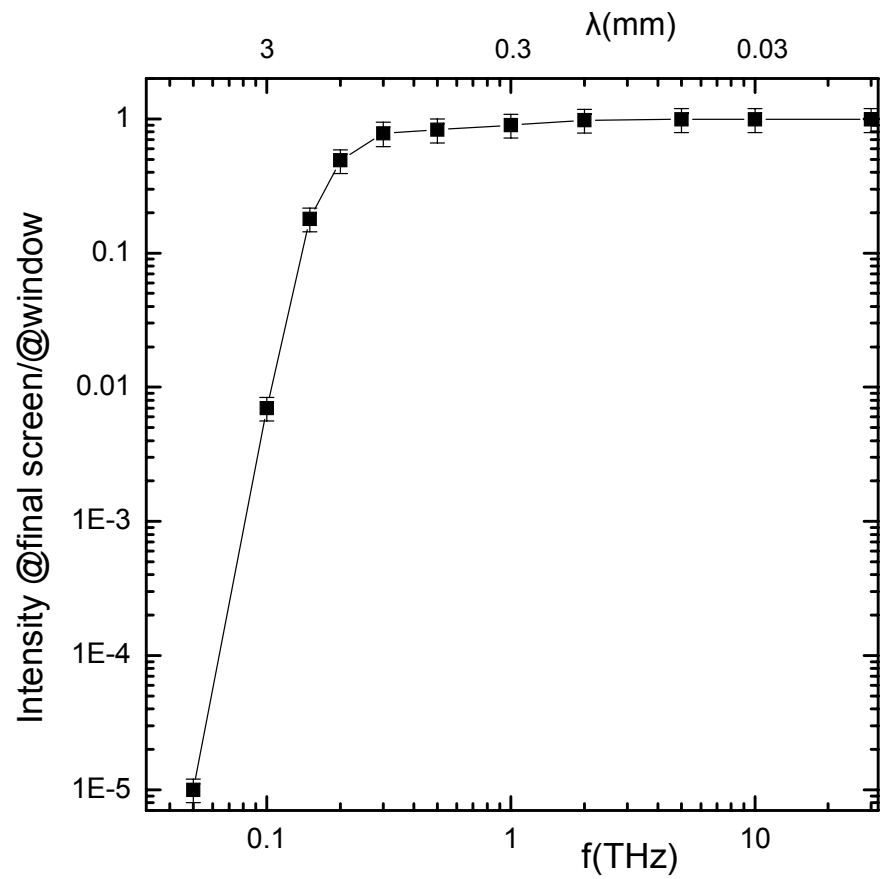
$\gamma = 1000$

CTR screen $\phi = 25\text{mm}$

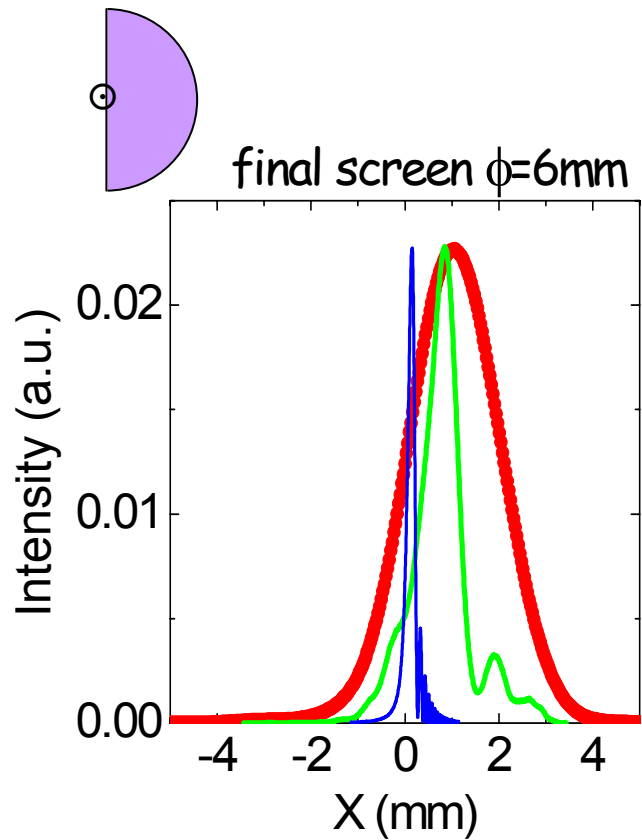
diamond window $\phi = 20\text{mm}$

	λ (mm)	f (THz)	Intensity @final screen/@window
●	1.5	0.2	0.49
—	0.3	1	0.90
—	0.01	30	0.99

Transfer function

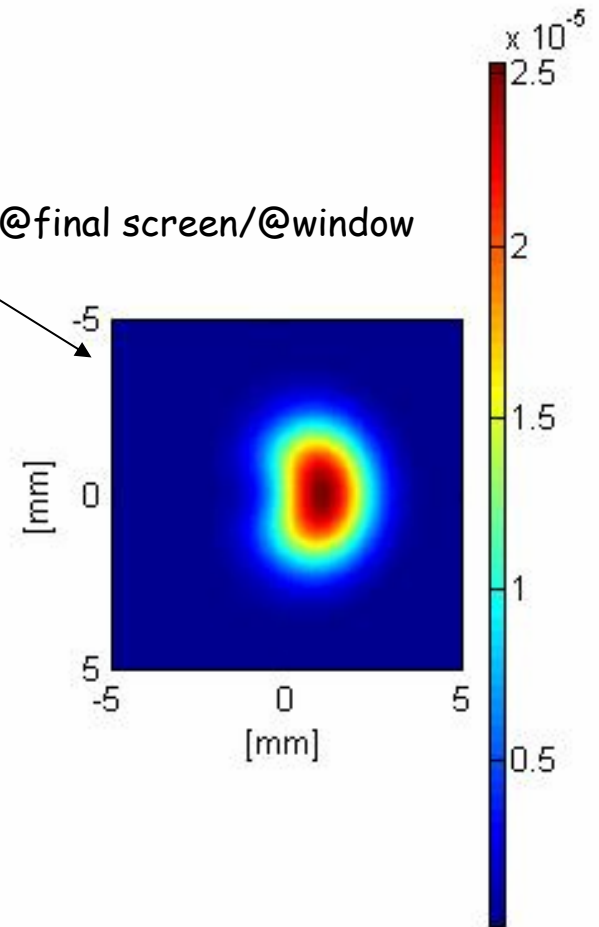


Half screen and horizontal polarization: frequency response

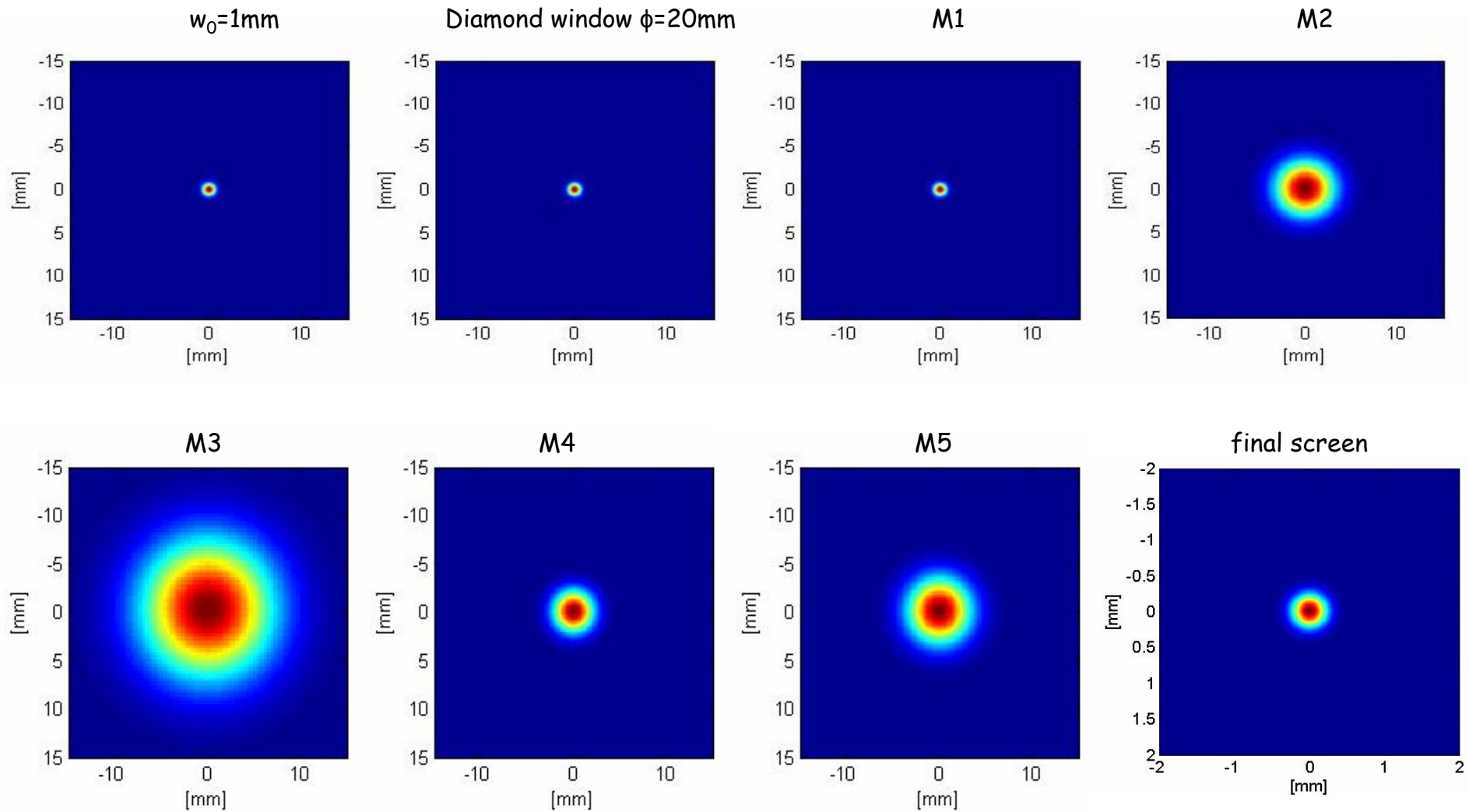


$\gamma = 1000$
 CTR screen $\phi = 25\text{mm}$
 diamond window $\phi = 20\text{mm}$

λ (mm)	f (THz)	Intensity @final screen/@window
1.5	0.2	0.52
0.3	1	0.91
0.01	30	0.99



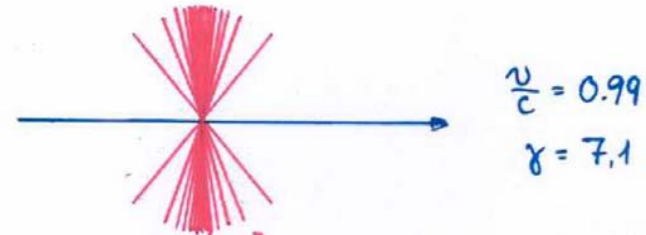
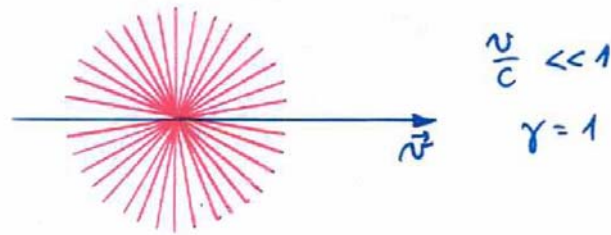
Gaussian beam $\lambda=500\text{nm}$



Summary and outlook

- 2 simulation tools: very good agreement
- Optical design for the THz beam line transfer @140m in TTF2: tested for CTR, CDR and Gaussian beam
- Outlook
 - "ideal" mirror surface
 - tests for stability against beam displacement and mirrors misalignment
 - effect of tilting CTR screen

Electric field of a charge in the laboratory system



$$\vec{E}(\vec{r}) = \frac{q}{4\pi\epsilon_0} \cdot \frac{(1-\beta^2)}{(1-\beta^2 \sin^2 \theta)^{3/2}} \cdot \frac{\vec{r}}{r^3}$$

$$E_z \cong 0; \quad E_r = \frac{q}{4\pi\epsilon_0} \cdot \gamma \cdot \frac{r}{[\gamma^2(z-vt)^2 + r^2]^{3/2}}$$

$$\zeta = z - vt = z - \beta ct$$

$$\tilde{E}_r(k, r) = \int_{-\infty}^{\infty} E_r(k, r) \cdot e^{ik\zeta} d\zeta$$

$$\tilde{E}_r(k, r) = \frac{q}{4\pi\epsilon_0} \cdot \frac{k}{\gamma} \cdot K_1\left(\frac{kr}{\gamma}\right)$$

